NASA/TM-2001-210891



Temperature Measurement of Beryllia Ceramic Surface in the Presence of Reflected Extraneous Radiation Using a Multiwavelength Pyrometer

Daniel Ng and Gustave Fralick Glenn Research Center, Cleveland, Ohio Since its founding, NASA has been dedicated to the advancement of aeronautics and space science. The NASA Scientific and Technical Information (STI) Program Office plays a key part in helping NASA maintain this important role.

The NASA STI Program Office is operated by Langley Research Center, the Lead Center for NASA's scientific and technical information. The NASA STI Program Office provides access to the NASA STI Database, the largest collection of aeronautical and space science STI in the world. The Program Office is also NASA's institutional mechanism for disseminating the results of its research and development activities. These results are published by NASA in the NASA STI Report Series, which includes the following report types:

- TECHNICAL PUBLICATION. Reports of completed research or a major significant phase of research that present the results of NASA programs and include extensive data or theoretical analysis. Includes compilations of significant scientific and technical data and information deemed to be of continuing reference value. NASA's counterpart of peerreviewed formal professional papers but has less stringent limitations on manuscript length and extent of graphic presentations.
- TECHNICAL MEMORANDUM. Scientific and technical findings that are preliminary or of specialized interest, e.g., quick release reports, working papers, and bibliographies that contain minimal annotation. Does not contain extensive analysis.
- CONTRACTOR REPORT. Scientific and technical findings by NASA-sponsored contractors and grantees.

- CONFERENCE PUBLICATION. Collected papers from scientific and technical conferences, symposia, seminars, or other meetings sponsored or cosponsored by NASA.
- SPECIAL PUBLICATION. Scientific, technical, or historical information from NASA programs, projects, and missions, often concerned with subjects having substantial public interest.
- TECHNICAL TRANSLATION. Englishlanguage translations of foreign scientific and technical material pertinent to NASA's mission.

Specialized services that complement the STI Program Office's diverse offerings include creating custom thesauri, building customized data bases, organizing and publishing research results . . . even providing videos.

For more information about the NASA STI Program Office, see the following:

- Access the NASA STI Program Home Page at http://www.sti.nasa.gov
- E-mail your question via the Internet to help@sti.nasa.gov
- Fax your question to the NASA Access Help Desk at 301–621–0134
- Telephone the NASA Access Help Desk at 301–621–0390
- Write to:

NASA Access Help Desk NASA Center for AeroSpace Information 7121 Standard Drive Hanover, MD 21076

NASA/TM-2001-210891



Temperature Measurement of Beryllia Ceramic Surface in the Presence of Reflected Extraneous Radiation Using a Multiwavelength Pyrometer

Daniel Ng and Gustave Fralick Glenn Research Center, Cleveland, Ohio

National Aeronautics and Space Administration

Glenn Research Center

Available from

NASA Center for Aerospace Information 7121 Standard Drive Hanover, MD 21076 National Technical Information Service 5285 Port Royal Road Springfield, VA 22100

Temperature Measurement of Beryllia Ceramic Surface in the Presence of Reflected Extraneous Radiation Using a Multiwavelength Pyrometer

Daniel Ng and Gustave Fralick National Aeronautics and Space Administration Glenn Research Center Cleveland, Ohio 44135

Introduction

It is often advantageous to employ pyrometry to measure the temperature of a surface. However, reflected radiation originating from sources surrounding the surface of interest is inevitably also included into the measurement process. Inclusion of this extraneous radiation component will introduce erroneous result. This report discusses the use of a multiwavelength pyrometer in a laboratory experiment to measure the temperature of a beryllia ceramic tube surface heated by a propane torch flame while a copious amount of extraneous radiation produced by a quartz lamp was simultaneously reflected by the beryllia surface into the pyrometer (Fig. 1). The multiwavelength pyrometer successfully determined not only the temperature of the beryllia surface but also that of the quartz lamp filament.

Method and Results

Temperature measurements reported in this report are performed using a multiwavelength pyrometer. The multiwavelength pyrometer is configured to accept signals via a 20-meter long silica optical fiber. It is calibrated by a blackbody furnace set to a known temperature as indicated by type K thermocouples. For this experiment, the multiwavelength pyrometer was configured to work between approximately 0.5 to 2.5 μ m. At the shortest end of this spectral region, the calibrating blackbody furnace (whose temperature was at 1293.6 K) radiation has just sufficient intensity for the pyrometer's silicon detector to generate a barely detectable signal. Another detector also employed to cover the other end of this spectral range was a lead sulfide detector. After calibration, the radiation spectrum of the blackbody furnace was recorded using the multiwavelength pyrometer. This spectrum is shown in Fig. 2, where a good fitting Planck curve of that temperature is superimposed.

To introduce extraneous reflection radiation into our experiment, a nominal 100 W quartz lamp in a housing with a focusing lens and fiber output connector was used. The input end of the multiwavelength pyrometer's optical fiber was coupled to this output connector. The quartz lamp power supply was adjusted such that the quartz lamp generated only 60 W of power. A higher power supply setting resulted in the multiwavelength pyrometer detector becoming saturated. The recorded spectrum is shown in Fig. 3. The quartz lamp housing fiber connector fixture was next removed to allow the focusing lens to project a beam of quartz lamp radiation on the surface of the beryllia sample that was being studied. The sample was a beryllia ceramic tube that was used in the construction of the NASA designed gas temperature measurement probe (Ref. 1). The input end of the pyrometer's silica fiber was positioned at an angle to receive quartz lamp radiation being reflected by the beryllia surface into the multiwavelength pyrometer spectrometer. The recorded reflected radiation spectrum is shown in Fig. 4.

Later, this relative arrangement between the quartz lamp, the beryllia ceramic, and the multiwavelength pyrometer's input optical fiber was maintained and undisturbed, but the quartz lamp was not turned on. The beryllia ceramic was raised to an unknown high temperature using a propane torch flame. An emission spectrum of the beryllia ceramic was recorded, and is shown in Fig. 5. Maintaining the propane torch flame at the same intensity, the quartz lamp was turned back on to the same power supply setting as before. A radiation spectrum was again recorded. This spectrum consisted of radiation emitted by the hot

beryllia ceramic surface as well as quartz lamp radiation reflected by the beryllia ceramic surface. It is shown in Fig. 6.

Analysis and Discussions

We analyzed the quartz lamp radiation spectrum data in Fig. 3 according to the procedure we have employed (Ref. 1) by transforming Eqn. (1), which is Planck's law of blackbody radiation at temperature T

$$L_{\lambda}(T) = \varepsilon_{\lambda} \tau_{\lambda} \frac{c_{I}}{\lambda^{5}} \frac{1}{\exp(c_{2}/\lambda T) - I} = \varepsilon_{\lambda} \tau_{\lambda} \frac{c_{I}}{\lambda^{5}} \exp(-c_{2}/\lambda T) \frac{1}{I - \exp(-c_{2}/\lambda T)}$$
(1)

into the form

$$y = \left(\frac{\operatorname{Ln}\left(\frac{c_1}{\lambda^5} \frac{1}{L_{\lambda}}\right)}{c_2/\lambda}\right) - \frac{\operatorname{Ln}\left(1 - \exp\left(-\frac{c_2}{\lambda T}\right)\right)}{c_2/\lambda} = \frac{1}{T} - \frac{\lambda}{c_2} \operatorname{Ln}(\varepsilon_{\lambda} \tau_{\lambda})$$
(2)

where c_1 =2 π hc², c_2 =hc/k are the radiation constants, with c being the velocity of light, h Planck's constant, k Boltzmann's constant, L_{λ} the radiation intensity, ϵ_{λ} the emissivity of the radiation source, and τ_{λ} the transmissivity of the optical medium between the pyrometer and the radiation source at wavelength λ . The quartz lamp spectrum data (Fig. 3) is plotted according to Eq. (2) to produce a straight line in Fig. 7. From its intercept a temperature of 3200 K is obtained. It can be noticed that the data are well fitted by two straight lines having the same intercept, but possessing different slopes. These slopes are related to the combined effects of quartz lamp filament emissivity (ϵ_{λ}) and the total transmissivities (τ_{λ}) of the quartz lamp bulb envelope and the lamp housing's focusing lens whose products in the two spectral regions are almost constant. By similarly transformation and analysis of the spectrum in Fig. 5 according to Eq. (2) to fit a single straight line, from whose intercept the unknown beryllia ceramic temperature was determined to be 1230 K. The result is shown in Fig. 8.

In a general application environment, radiation from sources other than just the surface of interest is detected simultaneously by the pyrometer. Radiation of surfaces whose temperatures we seek to measure using a pyrometer will be inevitably corrupted by non-surface origin extraneous components, such as the spectrum in Fig. 6 reveals. The temperature determined would be incorrect. We will show how we can determine the temperature of surfaces even from corrupted radiation data.

By dividing the reflected intensities at each wavelength of the spectrum in Fig. 4 by the incident intensities of the corresponding wavelength of the spectrum in Fig. 3, a spectral reflectivity σ_{λ} of the beryllia ceramic surface is obtained (Fig. 9). It is obvious that the spectrum in Fig. 6 does not possess the Planck functional appearance because it contained contributions from both emitted and reflected sources whose temperatures are different. We represent it as S_{λ} , where

$$S_{\lambda} = g \left[\varepsilon_{\lambda} L_{\lambda} (T_{s}) + \sigma_{\lambda} L_{\lambda} (T_{e}) \right]$$
 (3)

$$\varepsilon_{\lambda} = 1 - \sigma_{\lambda}$$
 (4)

where T_s is the unknown surface temperature, T_e is the temperature of the extraneous quartz lamp radiation source, and g is a geometric factor related to any change which the pyrometer's optical arrangement (in position and orientation) might have undergone between calibration and when it was finally used in the experiment.

The reflectivity σ_{λ} , and hence also ϵ_{λ} , are experimentally determinable, known quantities. Using different value sets of (T_e, T_s, g) , Eq. (3) is calculated. The minimum value of the sum of squares of the differences between the calculated (according to Eq. (3)) and the experimentally measured quantities (the spectrum of Fig. 6) was found to be 0.0506 for the N=440 wavelength channels. The values of T_e and T_s which produced this minimum were the temperatures we sought. They were 3252 K and 1233.6 K respectively. They were thus the best estimates of the quartz lamp filament and the beryllia ceramic surface temperatures obtainable from the data in Fig. 6. These temperatures were in excellent agreement (respectively within 1.6 % and 0.3 %) with the temperatures determined from the non-contaminated spectra in Figs. 3 and 5. A best estimate of the value of g was also obtained, but its significance and value does not concern us here.

Conclusion

The temperature of a beryllia ceramic surface, subjected to extraneous radiation illumination was measured using the multiwavelength pyrometer by decomposing the measured radiation spectrum into the constituent parts. A one time, pre-experiment measurement of beryllia reflectivity was used. This reflectivity measurement is not necessary for materials whose reflectivity does not vary drastically with wavelength when the use of an adjustable unknown fitting parameter would be sufficient. Ordinary 1- and 2-color pyrometers are unable to measure the correct temperature under the present conditions where the pyrometer signal is corrupted. This method we have described would be very valuable for in situ measurement of turbine blades temperature, when the blades are located close to the vicinity of the combustion chamber where the combustion fireball constantly illuminates the blades.

References

(1) Gustave Fralick and Daniel Ng, Pyrometric Gas and Surface Temperature Measurements, NASA/TM—1999-20959.

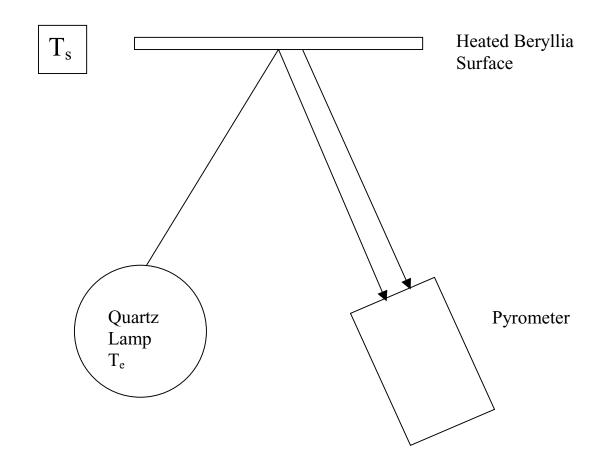


Fig. 1 Schematic of Experiment

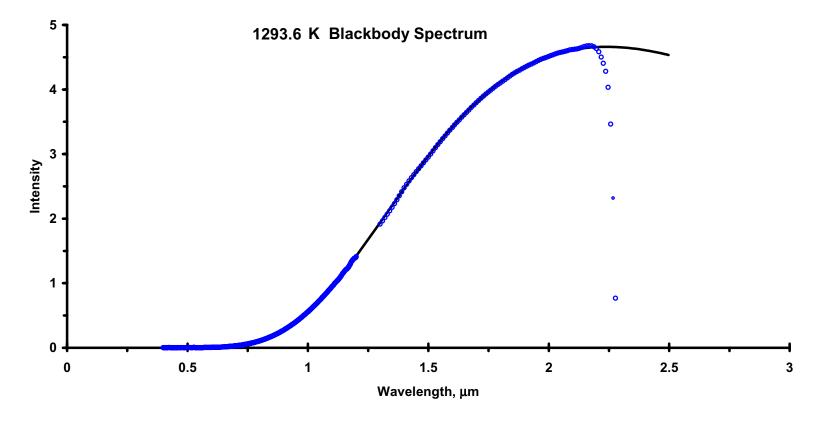


Fig. 2 Blackbody furnace spectrum. Symbols are data and solid line is the fitted line.

Quartz Lamp Spectrum T = 3200 K

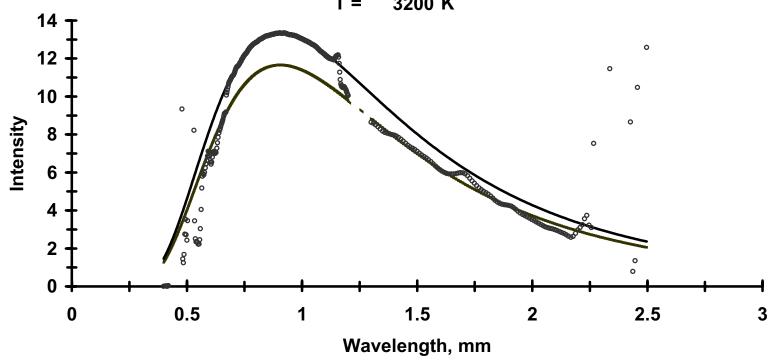


Fig 3. Quartz Lamp Radiation Spectrum

Reflected Quartz Radiation

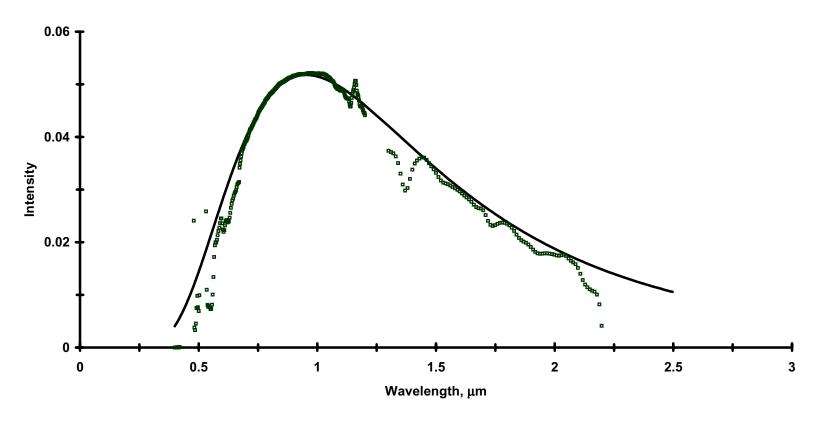


Fig. 4 Beryllia Ceramic Reflected Quartz Lamp Spectrum

BeO Emission Spectrum

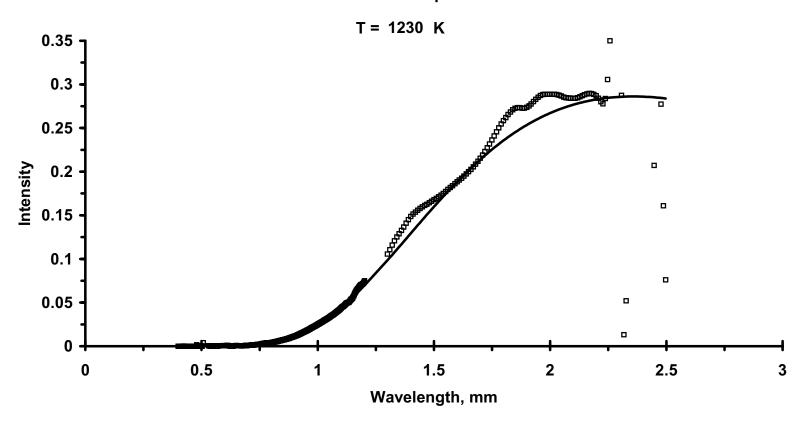


Fig. 5 Propane Torch Heated Beryllia Ceramic Surface Emission Spectrum

Emission plus Reflection

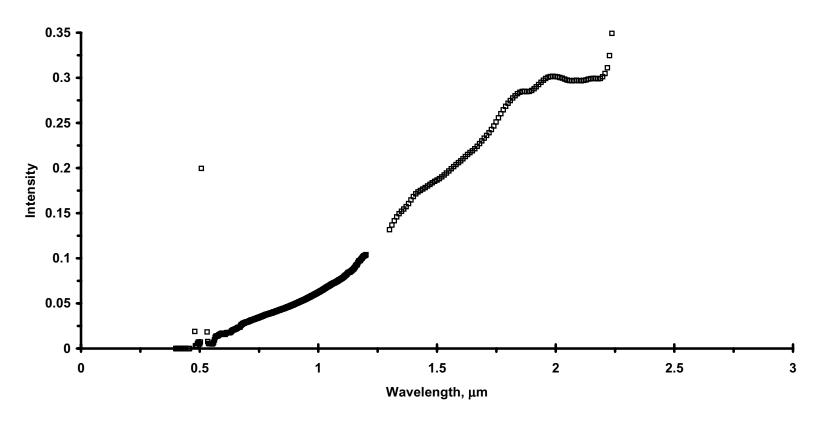


Fig. 6 Propane Torch Heated Beryllia Ceramic Surface Emission Spectrum Plus Reflected Quartz Lamp Radiation.

Fit Quartz Lamp Temperature T = 3200 K 0.0007 0.0005 0.0003 0 0.5 1 1.5 2 2.5

Fig. 7 Quartz lamp temperature determination from the reciprocal of the intercept.

 $\textbf{WAVELENGTH}, \, \mu \textbf{m}$

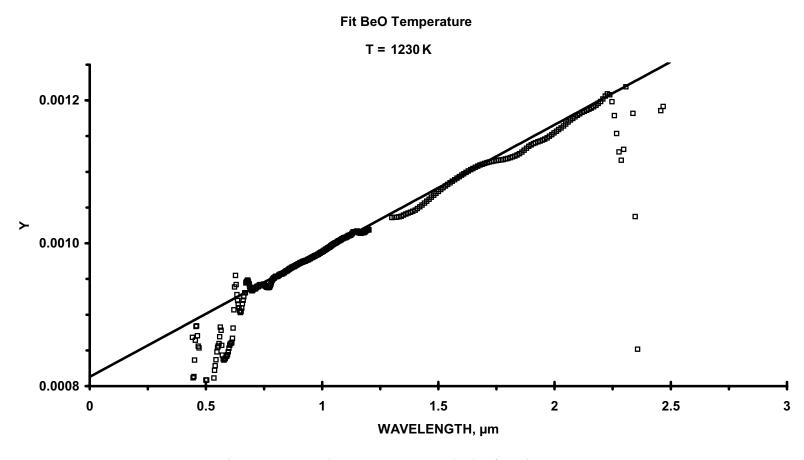


Fig. 8 BeO ceramic Temperature Determination from the Intercept.

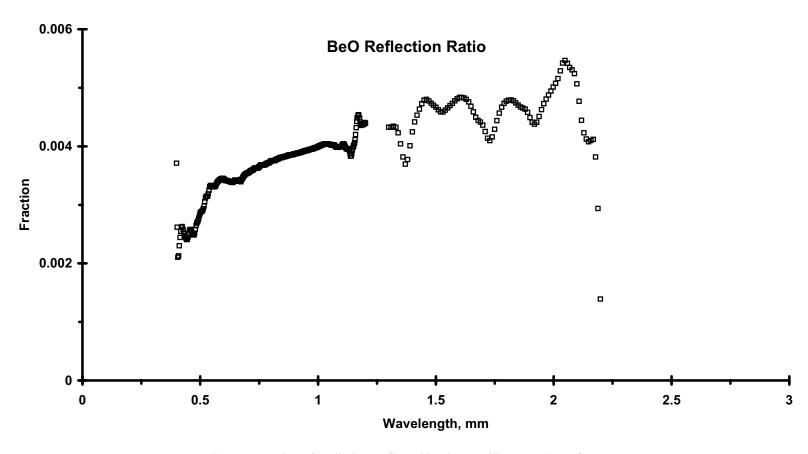


Fig. 9 Fraction of Radiation Reflected by the Beryllia Ceramic Surface.

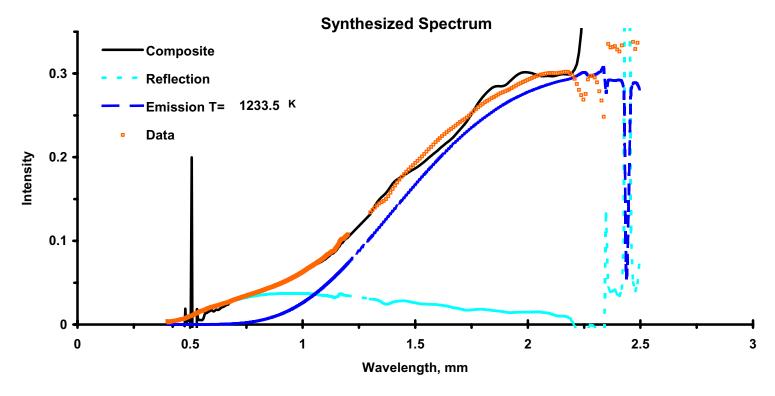


Fig. 10 Synthesis of the Spectrum in Fig. 6 from two components.

REPORT DOCUMENTATION PAGE

Form Approved OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.

1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE	3. REPORT TYPE AND DATES COVERED	
	May 2001	Te	chnical Memorandum
4. TITLE AND SUBTITLE 5. FUN			5. FUNDING NUMBERS
Temperature Measurement of Beryllia Ceramic Surface in the Presence of Reflected Extraneous Radiation Using a Multiwavelength Pyrometer			WHI 700 20 20 00
6. AUTHOR(S)			WU-728-30-20-00
Daniel Ng and Gustave Fralick			
			8. PERFORMING ORGANIZATION
National Aeronautics and Space Administration John H. Glenn Research Center at Lewis Field Cleveland, Ohio 44135–3191			E-12767
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) 10. S			10. SPONSORING/MONITORING
			AGENCY REPORT NUMBER
National Aeronautics and Space Administration Washington, DC 20546–0001			NASA TM—2001-210891
11. SUPPLEMENTARY NOTES			
Responsible person, Daniel Ng, organization code 5510, 216–433–3638.			
12a. DISTRIBUTION/AVAILABILITY	STATEMENT		12b. DISTRIBUTION CODE
Unclassified - Unlimited Subject Category: 35	Distrib	ution: Nonstandard	
Available electronically at http://gltrs.grc.nasa.gov/GLTRS This publication is available from the NASA Center for AeroSpace Information, 301–621–0390.			
13. ABSTRACT (Maximum 200 words)			
originating from sources sur Inclusion of this extraneous multiwavelength pyrometer heated by a propane torch fl neously reflected by the ber	radiation component will introd in a laboratory experiment to m ame while a copious amount of	is inevitably also includ luce erroneous result. The easure the temperature of extraneous radiation pro The multiwavelength py	ed into the measurement process. is report discusses the use of a of a beryllia ceramic tube surface oduced by a quartz lamp was simulta- yrometer successfully determined not
14 CHD IECT TEDMO			45 NUMBER OF BACES
14. SUBJECT TERMS			15. NUMBER OF PAGES
Pyrometry; Temperature; Beryllia; Ceramic			16. PRICE CODE
17. SECURITY CLASSIFICATION OF REPORT Unclassified	18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified	19. SECURITY CLASSIFICA OF ABSTRACT Unclassified	TION 20. LIMITATION OF ABSTRACT
CHCIASSILICU	CHCIASSILIEU	i Uniciassified	· · · · · · · · · · · · · · · · · · ·